



# **Electron Sources**

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**USPAS 08**

**U. of Maryland, College Park**



# Electron Sources in General



TYPE & Max. Current Density	PHYSICS	TYPICAL CONFIG.	APPLICATIONS
Thermionic Up to 1 A/cm <sup>2</sup>	Richardson- Dushman, Child-Langmuir	Cathode + Electron Gun	Microwave tubes, Incoherent X-Ray sources, etc.
Photoemiss. >> 1 A/cm <sup>2</sup>	Photoelectric effect	RF Photocathode	Many accelerators, FELs, etc.
Field- Emission >>> 1 A/cm <sup>2</sup>	Fowler- Nordheim	Cold-cathode, Needle	Discharge tubes, Field-Effect Microscopes
Other: Plasma, multipactor, nano-tube, laser cooled, etc	Laser cooling, nano-physics, etc.	Plasma Ion source, cavity, optical trap, etc.	Most under R&D



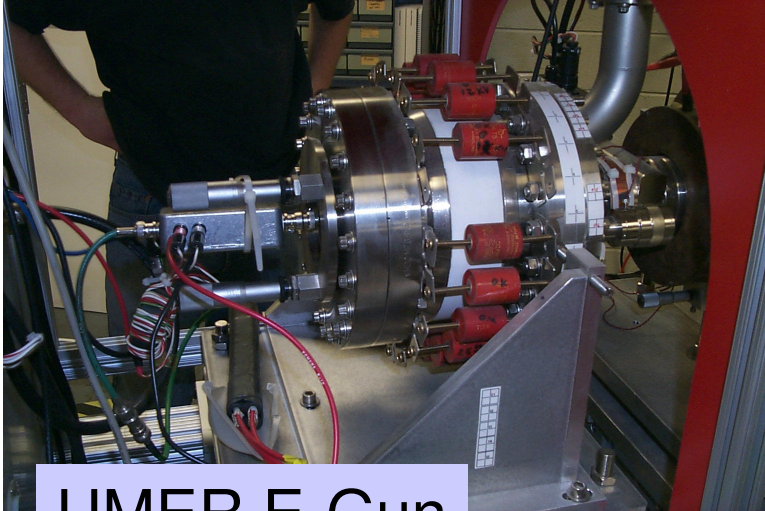
# Electron Sources in UMER Lab



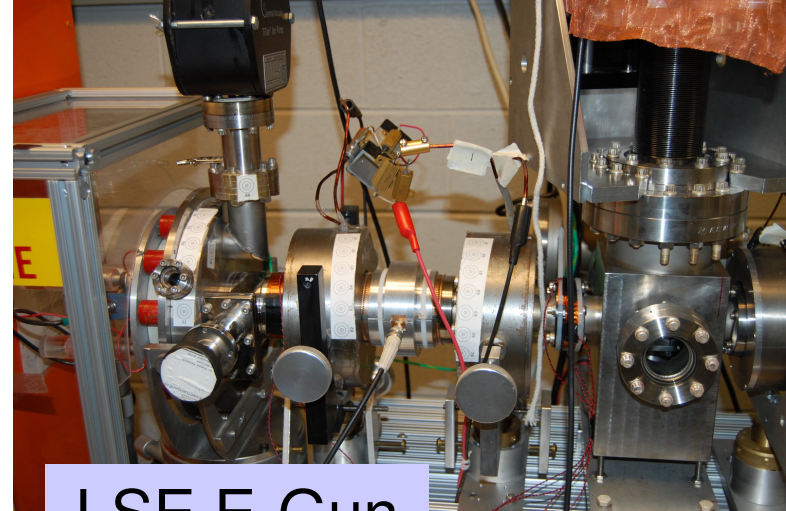
SOURCE	Max. Energy, Current, pulse	TYPE	DESCRIPTION
Hughes Gun $r_C = 12.7 \text{ mm}$	8 keV, 200 mA, $1 \mu\text{s}$	Pierce Geom., Convergent, diode	Scaled-down replica of SLAC PEP gun
LSE Gun $r_C = 4 \text{ mm}$	5 keV, 120 mA 100 ns	Pierce Geom., triode	Cathode-driven, Variable A/K gap
UMER Gun $r_C = 4 \text{ mm}$	10 keV, 100 mA, 100 ns	Pierce Geom., triode	Cathode-driven, Variable A/K gap



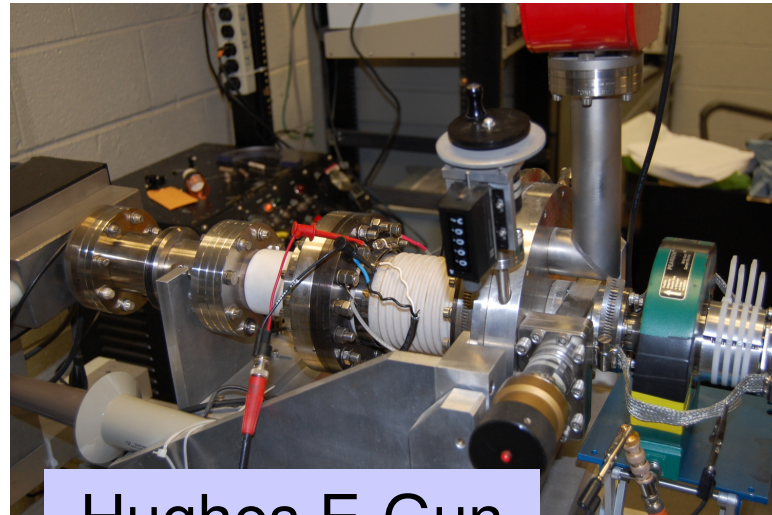
# Electron Sources in UMER Lab



UMER E-Gun



LSE E-Gun



Hughes E-Gun



# Physics of Thermionic Emiss. and Diode E-Guns



**Richardson-Dushman Equation<sup>1</sup>:**

$$j_{CM} = AT_C^2 \exp\left(-\frac{qW}{k_B T_C}\right),$$

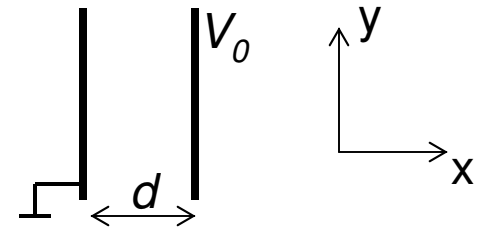
$$T_C = 1373\text{K}, A = 1.2 \times 10^6 \frac{\text{Amp}}{\text{m}^2\text{K}^2}, W = 2.1\text{V}.$$

**Child-Langmuir<sup>2</sup>:**

$$j_{CL} = \frac{4}{9} \epsilon_0 \left(\frac{2q}{M}\right)^{1/2} \frac{V_0^{3/2}}{d^2},$$

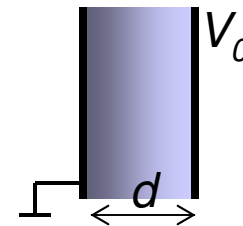
**1-D diode w/o space charge:**

$$\phi(x) = V_0 \left(\frac{x}{d}\right).$$



**1-D diode with space charge:**

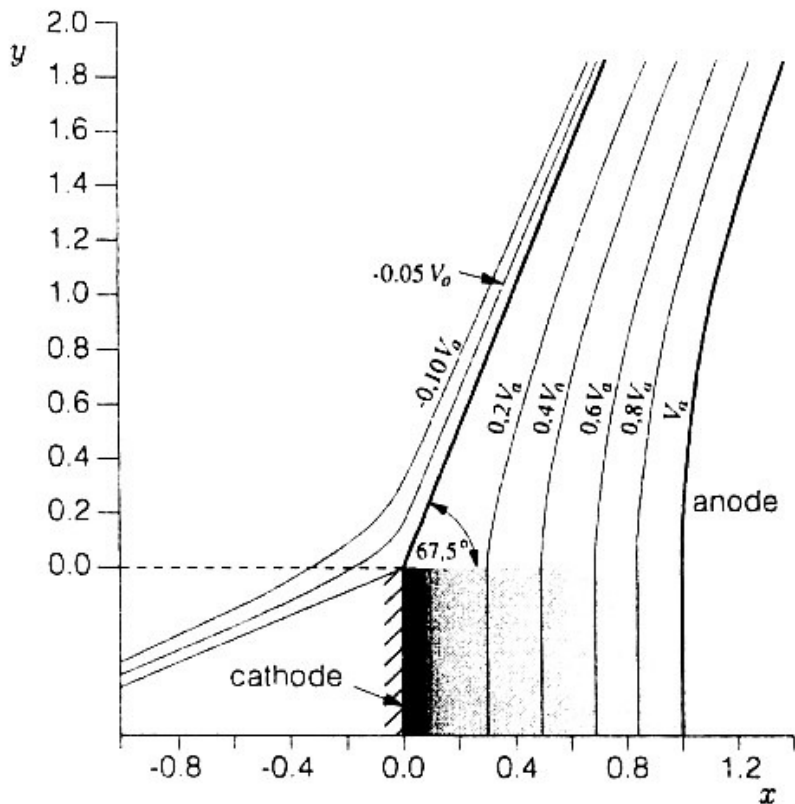
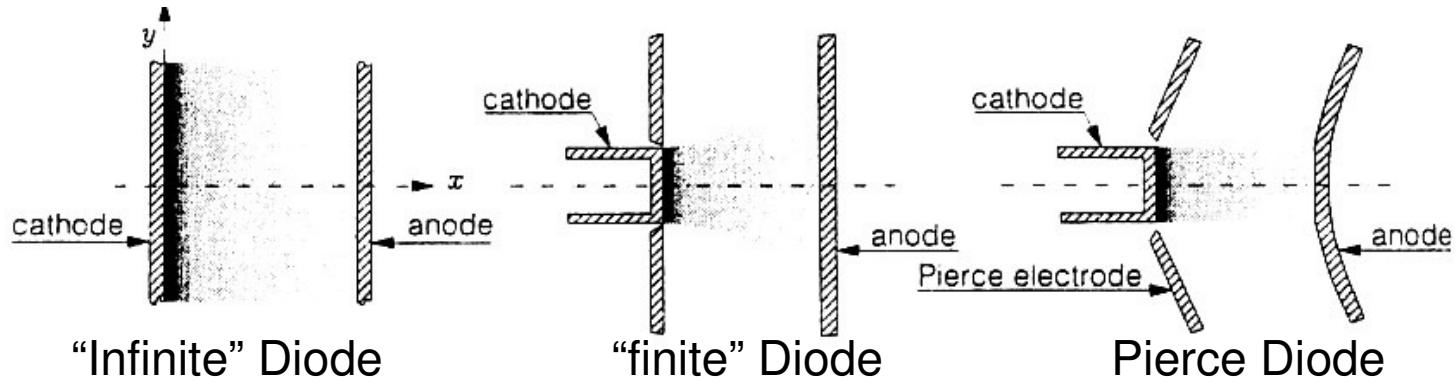
$$\phi(x) = V_0 \left(\frac{x}{d}\right)^{4/3}.$$



<sup>1</sup>See, for example, Leighton, Principles of Modern Physics, McGraw-Hill, 1959, p.355-56

<sup>2</sup>See Martin Reiser, Theory and Design of Charged Particle Beams, Sec. 2.5.2.

# Pierce Electrode Geometry\*



Assume  $V(x) \propto x^{4/3}$ , outside beam for finite (in y-direction) diode.

Use complex formalism  $x \rightarrow re^{i\phi} = \zeta + i\xi$ ,  
 $V \rightarrow W = V_R + iV_I$ .

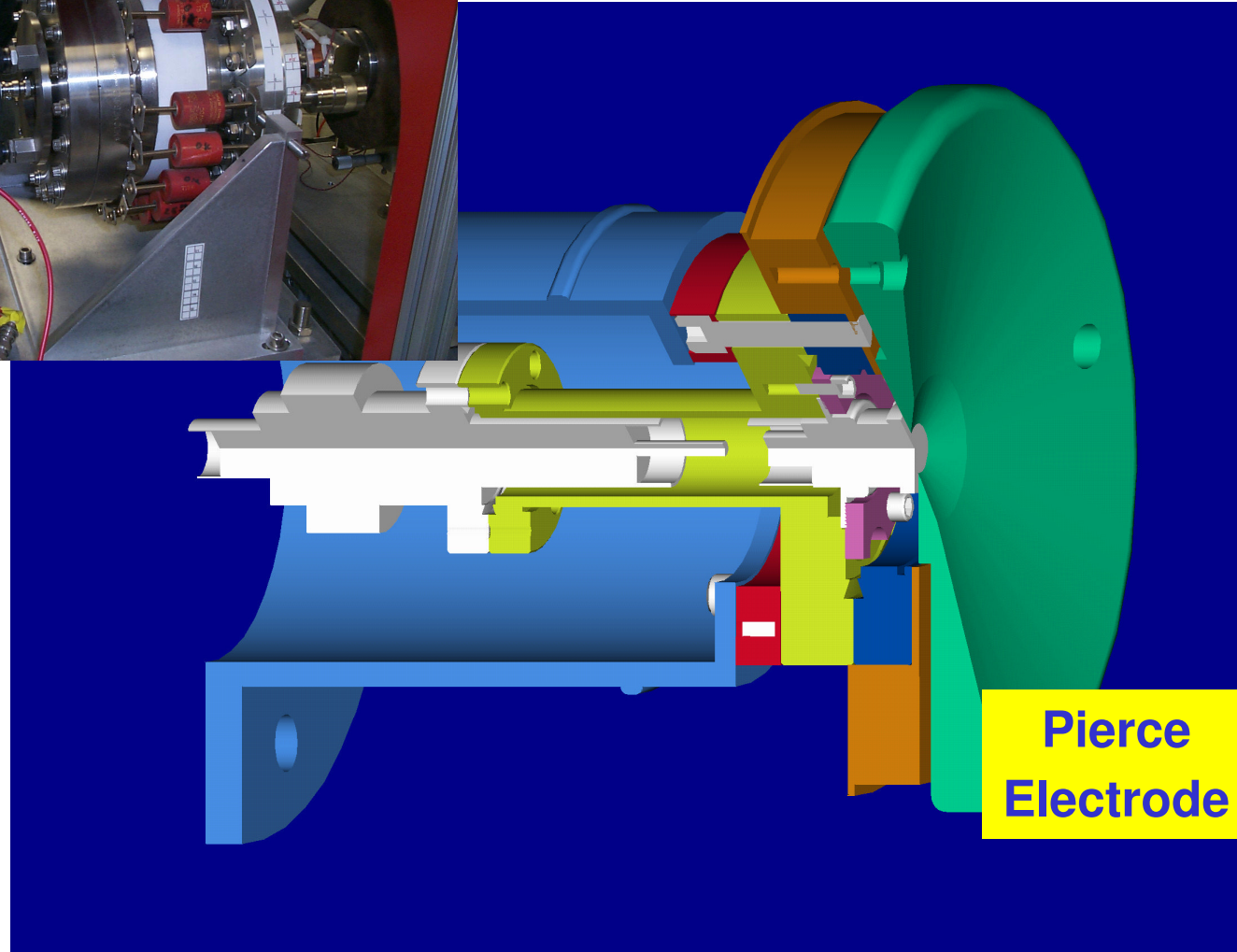
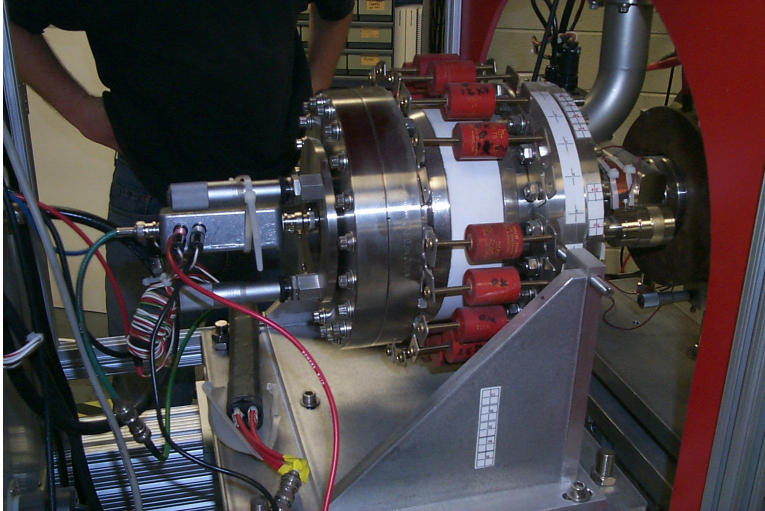
Then  $V_R \propto r^{2/3} \cos[(4/3)\arctan(\zeta/\xi)]$ .

Since cathode is grounded,  $V_R = 0$ , so we need  
 $(4/3)\arctan(\zeta/\xi) = \pi/2$ , or slope at  $x=0$  is

$$(3/4) \pi/2 = 67.5^\circ$$

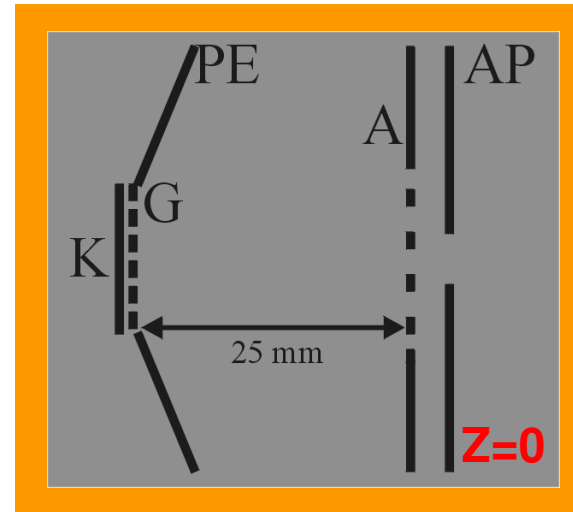
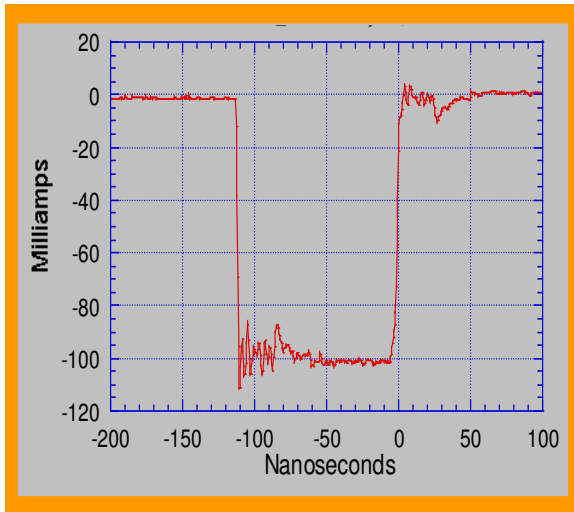
\*Miroslav Sedlacek, Electron Physics of Vacuum and Gaseous Devices, Sec. 6.2 (1996).

# UMER Electron Gun

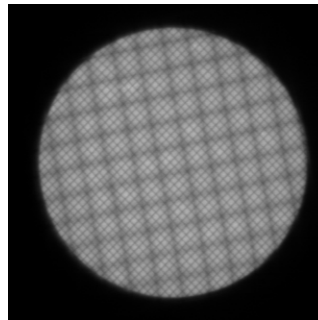


# UMER Electron Gun

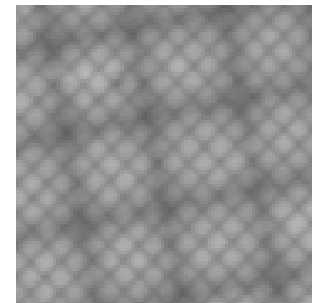
**TRIODE ELECTRON GUN: CATHODE DRIVEN, PIERCE TYPE**



**CATHODE  
AND  
ANODE GRIDS**

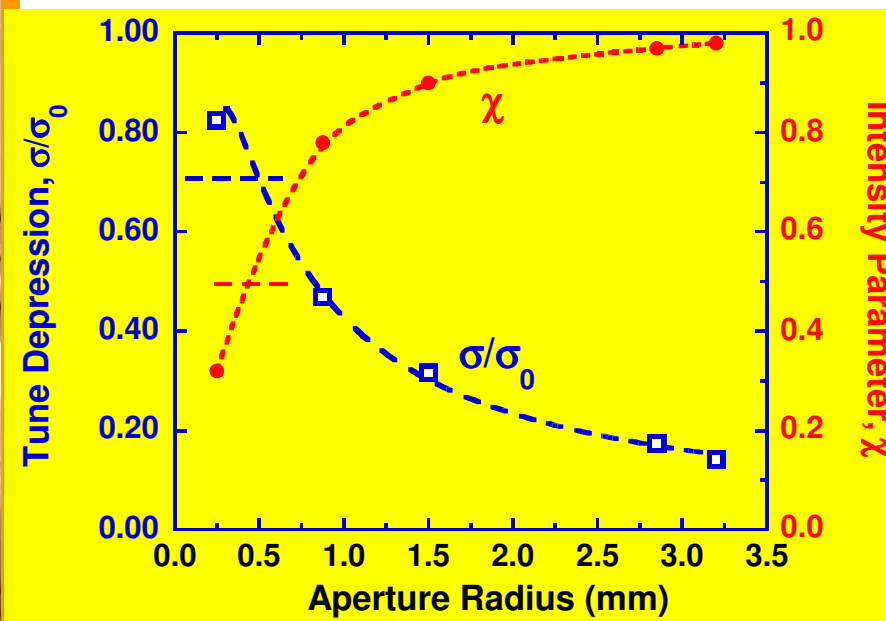
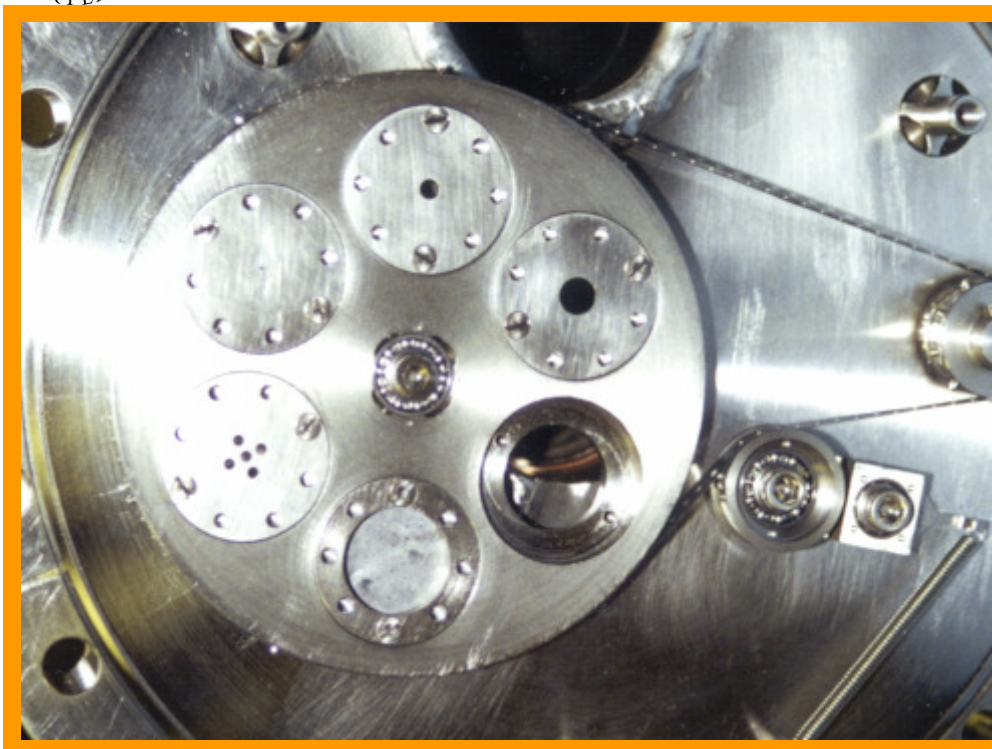


8 mm





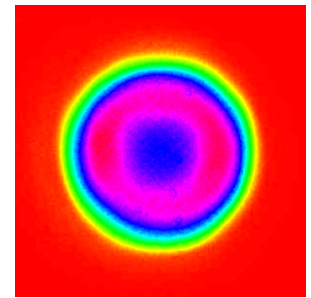
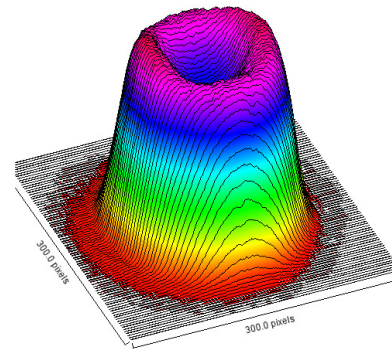
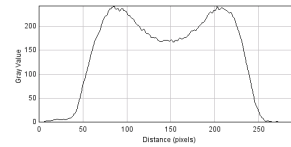
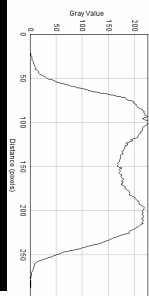
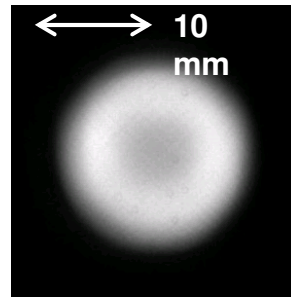
# UMER e-Gun Apertures



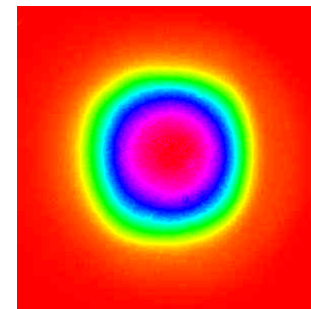
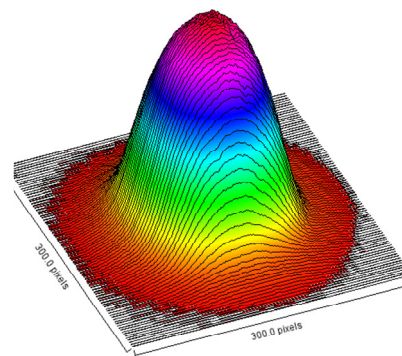
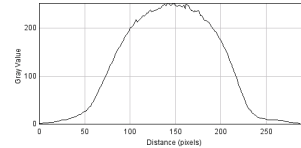
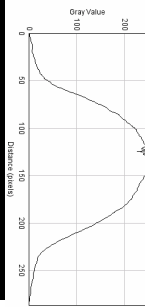
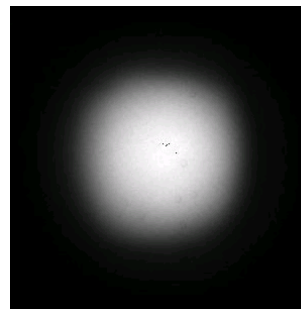
Aperture Radius	Beam Current	$\mathcal{M}$ ( $\text{\AA m}$ ) rms, norm.	$\chi$
0.25 mm	0.55 mA	$0.3 \pm 20\%$	0.28
0.875	7.2	0.7	0.81
1.5	24	1.5	0.90
2.85	85	2.7	0.97
Full	107	3.0	0.98

# Adjusting the E-Gun Control Grid Bias for Optimal Output

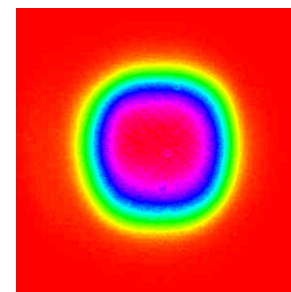
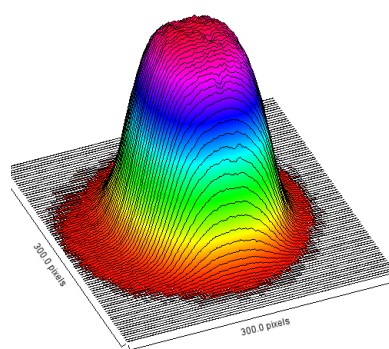
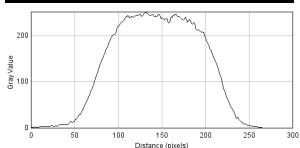
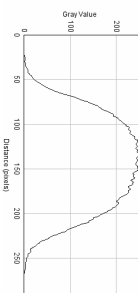
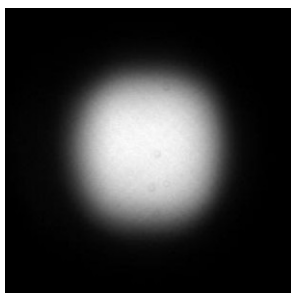
Ap=50  
BV=30V  
Sol=0  
No Atten.



Ap=50  
BV=45V  
Sol=0  
No Atten.



Ap=50  
BV=42.2V  
Sol=0  
No Atten.



6.2 mA,  
10 keV